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## Article

# Quadratic Admissibility for a Class of LTI Uncertain Singular Fractional-Order Systems with $0 < \alpha < 2$

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**Abstract:** This paper provides a unified framework for the admissibility of a class of singular fractional-order systems with a given fractional order in the interval  $(0, 2)$ . These necessary and sufficient conditions are derived in terms of linear matrix inequalities (LMIs). The considered fractional orders range from 0 to 2 without separating the ranges into  $(0, 1)$  and  $[1, 2)$  to discuss the admissibility. Moreover, the uncertain system with the fractional order in the interval  $(0, 2)$  is norm-bounded. The quadratic admissibility and general quadratic stability of the system are analyzed, and the equivalence between the two is proved. All the above can be expressed in terms of strict LMIs to avoid any singularity problem in the solution. Finally, the effectiveness of the method is illustrated by three numerical examples.

**Keywords:** singular fractional-order systems; admissibility; linear matrix inequality; unified criterion



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## 1. Introduction

Fractional-order systems (FOSs) have received extensive attention in the field of natural science and applied engineering [1,2] in recent years and have gradually become a research hot spot because of their many practical backgrounds and engineering requirements. In order to conform to the actual research situation, the current research expands results from classical calculus [3,4] to fractional calculus [5,6]. Indeed, FOSs are used to represent the nonclassical phenomena of various types of physical systems; FOSs have gradually become the main research object in the control field.

For all systems, stability is a prerequisite for the proper functioning of control systems in practical applications, let alone in FOSs. However, the stability analysis of FOSs [7,8] cannot be derived directly from integer-order systems (IOSs) [9,10] due to the complexity of their operators, and thus the stability of FOSs has become a hot topic of discussion in recent years. Li and Yu [11,12] proposed the definition of the Mittag–Leffler stability and introduced the fractional Lyapunov direct method to study the stability of fractional-order nonlinear dynamical systems. Lu and Chen [13] discussed the system matrix with interval uncertainties and analyzed the problem of the robust asymptotic stability of systems, where the order  $\alpha$  is in the interval  $(0, 1)$ . In [14], Semary confirmed the relationship between the stability of FOSs and the number of poles and investigated the stability of these systems by discussing the time-domain response based on the Mittag–Leffler function. Alagoz [15] analyzed the stability of FOSs by studying the root trajectories of expanded degree integer-order polynomials in the main Riemann table and using the properties of power maps. Kharade and Wang [16,17] studied the generalized Mittag–Leffler–Hyers–Ulam stability, which is crucial for the analysis of quadratic fractional integral equations. Abu-Shady and Kaabar [18,19] studied a generalized fractional derivative formulation called Abu-Shady–Kaabar fractional derivative, which could obtain the same results as from a Caputo fractional operator in a very simple way without modification or complex numerical techniques. Ibrir and Farges [20,21] proposed different forms of linear matrix

inequalities (LMIs) to solve the stability and stabilization problems of FOSs. In [22], Zhang and Lin provided a unified form of discrimination method for the stability and stabilization of FOSs with a fractional order in the interval  $(0, 2)$ .

Singular FOSs are a special class of FOSs for which it is necessary to ensure not only that they are stable, but also that they are regular and impulse-free, i.e., admissible [23–25]. In [26], Yu and Jiao discussed the admissibility of singular fractional order regular systems when the fractional order  $\alpha$  was  $0 < \alpha < 1$ . However, there were restrictions on the regularity of the system. The output feedback control problem of singular FOSs, including standardization and stabilization, was studied in [27]. Zhang and Marir [28,29] discussed the admissibility criteria of singular FOSs with order  $(0, 1)$  and  $[1, 2)$ , respectively, based on LMIs. Based on a Kronecker equivalent standard form, the properties of time-domain solutions of singular FOSs were analyzed, and the admissible criteria of singular FOSs were given [30–32]. The quadratic admissibility problem for a class of singular fractional-order linear time-invariant systems with fractional order  $1 < \alpha \leq 2$  was investigated, and then a static output feedback controller was designed for uncertain closed-loop systems [33]. Li and Zhang [34,35] ensured the admissibility of T-S fuzzy singular FOSs with fractional order  $0 < \alpha < 1$  by designing sliding-mode observers and proportional–differential dynamic compensators. Li et al. [36–38] designed suitable filters or controllers based on the bounded real Lemma of singular FOSs to ensure the admissibility of systems. In [39], Wei and Wang studied an LMI in the case of output feedback, but it needed to know the information of state variables, which may be troublesome in practical operation. The sliding-mode control problem for a class of singular FOSs with state matrix and derivative matrix uncertainties was studied by using radial basis function neural networks [40]. However, for singular FOSs, few works have dealt with the admissibility analysis with uncertainties, and the methods of studying uncertain systems are still being explored and studied [41,42]. In [43,44], based on the backstepping method, the fault-tolerant tracking control problem for a class of strict feedback nonlinear systems was studied. In practice, many uncertainties are bounded, but the literature on norm-bounded uncertainties is relatively scarce. Therefore, papers analyze singular FOSs with norm-bounded uncertainties and give quadratic admissibility criteria for such systems. For singular systems, many papers derive the admissibility criteria based on nonstrict LMIs, which lead to huge errors in numerical simulation due to equality constraints. However, the results given in this paper addresses the above problems through a strict LMI form which can quickly find feasible solutions.

Based on the above observations, the admissibility and quadratic admissibility of a class of linear time-invariant (LTI) singular FOSs are studied. Different from existing methods, the main contributions of this paper are as follows:

(i) This unified LMI framework is applicable to singular FOSs with an order in  $(0, 2)$ , instead of separating the order, as in the existing literature, into  $(0, 1)$  or  $[1, 2)$  to discuss them separately.

(ii) In this paper, the admissibility criterion of an LMI is given; the criterion includes a nonstrict form and strict form, which can ensure that the singularity problem does not occur.

(iii) For singular FOSs with a bounded norm, it is proved that the generalized quadratic stability and quadratic admissibility can be deduced from each other, and the conclusions in this paper can be extended to variable-order singular FOSs of order in  $(0, 2)$ .

The rest of this paper is organized as follows. Section 2 presents some existing results and preliminaries. Subsequently, the admissibility criteria for orders  $0 < \alpha < 2$  are obtained, and the main results are drawn in Section 3. Three numerical examples are given in Section 4 to illustrate the effectiveness of the results, and Section 5 describes the conclusions on the obtained results.

Within this work, we use the following notations:  $\lceil \alpha \rceil$  ( $\lfloor \alpha \rfloor$ ) represents the smallest (greatest, respectively) integer greater (less) than or equal to  $\alpha$ . The notation  $N^T$  represents the transpose of the matrix  $N$ ,  $\text{sym}(N)$  stands for  $\frac{1}{2}(N + N^T)$ ,  $\text{asym}(N)$  denotes the expression  $\frac{1}{2}(N - N^T)$ .  $\otimes$  indicates the Kronecker product of two matrices  $A$  and  $B$ , which is

defined as  $A \otimes B = [a_{ij}B]$ . \* denotes the matrix symmetric part.  $\arg(z)$  is the argument of a complex number  $z$ , and  $\text{spec}(E, A)$  is the spectrum of the pair  $(E, A)$ .

## 2. Problem Formulation and Preliminaries

Consider the singular FOS described as:

$$ED^\alpha x(t) = Ax(t) + Bu(t), \quad (1)$$

where  $x(t) \in \mathbb{R}^n$  is the pseudostate,  $u(t) \in \mathbb{R}^p$  is the control input,  $E \in \mathbb{R}^{n \times n}$  is singular with  $\text{rank}(E) = r < n$ ,  $A \in \mathbb{R}^{n \times n}$  and  $B \in \mathbb{R}^{n \times p}$  are constant matrices. The symbol  $D^\alpha$  is the fractional differentiation operator of order  $\alpha$  of  $x(t)$ , which has the following three definitions. The Grünwald–Letnikov derivative:

$$D^\alpha x(t) = \lim_{h \rightarrow 0} h^{-\alpha} \sum_{j=0}^{\lfloor \frac{t-\alpha}{h} \rfloor} \omega_j^{(\alpha)} f(t - jh),$$

where

$$\omega_j^{(\alpha)} = \frac{(-1)^j \Gamma(\alpha + 1)}{\Gamma(j + 1) \Gamma(\alpha - j + 1)},$$

the Riemann–Liouville derivative:

$$D^\alpha x(t) = \frac{1}{\Gamma(m - \alpha)} \frac{d^m}{dt^m} \int_0^t (t - \tau)^{m - \alpha - 1} f(\tau) d\tau,$$

and the Caputo derivative:

$$D^\alpha x(t) = \frac{1}{\Gamma(\lceil \alpha \rceil - \alpha)} \int_0^t (t - \tau)^{\lceil \alpha \rceil - \alpha - 1} x^{(\lceil \alpha \rceil)}(\tau) d\tau,$$

where  $\Gamma(\cdot)$  is Euler's gamma function:

$$\Gamma(z) = \int_0^\infty t^{z-1} e^{-t} dt.$$

The Caputo derivative is widely used in the engineering field because its initial value conditions of differential equations are consistent with those of integral calculus. In this paper, the Caputo derivative is used to handle initial value conditions conveniently. In the rest of the text,  $D^\alpha$  solely represents the Caputo derivative.

Next, for the unforced singular FOS:

$$ED^\alpha x(t) = Ax(t); \quad (2)$$

when matrix  $E$  is nonsingular, especially when  $E$  is an identity matrix, system (2) is simplified to a normal FOS and is rewritten into the following form:

$$D^\alpha x(t) = Ax(t). \quad (3)$$

Let us recall some known facts on the unforced ( $u(t) \equiv 0$ ) system (2).

**Definition 1** ([23]). System (2) is said to be admissible if system (2) meets the following three conditions at the same time:

- (i) System (2) is regular, that is,  $\det(s^\alpha E - A) \neq 0$ ;
- (ii) System (2) is impulse-free, that is,  $\deg(\det(sE - A)) = \text{rank}(E)$ ;
- (iii) System (2) is stable, that is,  $|\arg(\text{spec}(E, A))| > \alpha \frac{\pi}{2}$ .

**Lemma 1** ([22]). System (3) with a given fractional order  $\alpha$  in the interval  $(0, 2)$  is stable iff there exists a matrix  $X \in \mathbb{R}^{n \times n}$  such that the following inequalities hold:

$$\begin{bmatrix} \text{sym}(X) & \text{asym}(X) \\ [\alpha - 1]\text{asym}(X) & \text{sym}(X) \end{bmatrix} > 0, \tag{4}$$

$$\text{sym}\{\Theta_\alpha \otimes (AX_\alpha)\} < 0, \tag{5}$$

where  $\Theta = \begin{bmatrix} \alpha_s & -\alpha_c \\ \alpha_c & \alpha_s \end{bmatrix}$ ,  $\alpha_s = \sin(\frac{\alpha\pi}{2})$ ,  $\alpha_c = \cos(\frac{\alpha\pi}{2})$ ,  $\Theta_\alpha = \Theta([\alpha])$ ,  $\Theta(1) = 1$ ,  $\Theta(2) = \Theta$ .  
 $X_\alpha = \alpha_s^{-[\alpha-1]} \cdot \text{sym}(X) + \alpha_c[\alpha - 1] \cdot \text{asym}(X)$ .

**Lemma 2** ([26]). For a given system (2), there exist two invertible matrices  $L, R \in \mathbb{R}^{n \times n}$  such that

$$LER = \begin{bmatrix} I_m & 0 \\ 0 & 0 \end{bmatrix}, LAR = \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix}, \tag{6}$$

where  $m = \text{rank}(E)$ .

If system (2) is regular, then system (2) is impulse-free iff  $A_{22}$  is invertible.

**Lemma 3** ([28]). System (2) with order  $\alpha$  in  $(0, 1)$  is admissible iff there exist two matrices  $X, Y \in \mathbb{R}^{n \times n}$  such that the following inequalities hold:

$$\begin{bmatrix} LERX & LERY \\ -LERY & LERX \end{bmatrix} = \begin{bmatrix} X^T(LER)^T & -Y^T(LER)^T \\ Y^T(LER)^T & X^T(LER)^T \end{bmatrix} \geq 0, \tag{7}$$

$$\text{sym}\{LAR(\alpha_s X - \alpha_c Y)\} < 0, \tag{8}$$

where  $L, R \in \mathbb{R}^{n \times n}$  are given by Lemma 2.

**Lemma 4** ([29]). System (2) with order  $\alpha$  in  $[1, 2)$  is admissible iff there exists matrix  $X \in \mathbb{R}^{n \times n}$  such that the following inequalities hold:

$$LERX = X^T(LER)^T \geq 0, \tag{9}$$

$$\text{sym}\{\Theta \otimes (LARX)\} < 0, \tag{10}$$

where  $L, R \in \mathbb{R}^{n \times n}$  are given by Lemma 2.

**Lemma 5** ([28]). System (2) with order  $\alpha$  in  $(0, 1)$  is admissible iff there exist four matrices  $X_1, X_4 \in \mathbb{R}^{m \times m}$ ,  $X_2 \in \mathbb{R}^{(n-m) \times m}$  and  $X_3 \in \mathbb{R}^{(n-m) \times (n-m)}$  such that the following inequalities hold:

$$\begin{bmatrix} X_1 & X_4 \\ -X_4 & X_1 \end{bmatrix} > 0, \tag{11}$$

$$\text{sym}\{\alpha_s LARX - \alpha_c LARY\} < 0, \tag{12}$$

where  $L, R \in \mathbb{R}^{n \times n}$  are given by Lemma 2, and

$$X = \begin{bmatrix} X_1 & 0 \\ X_2 & X_3 \end{bmatrix}, Y = \begin{bmatrix} X_4 & 0 \\ 0 & 0 \end{bmatrix}. \tag{13}$$

### 3. Main Results

In this section, uniform admissibility criteria for the singular FOSs are obtained, and quadratic admissibility criteria are given for the singular FOSs with norm-bounded uncertainties.

### 3.1. Admissibility of Unforced Linear Singular FOS with Order $0 < \alpha < 2$

The following results extend the order of the system to  $0 < \alpha < 2$  without any separation.

**Theorem 1.** System (2) is admissible iff there are  $X_1 \in \mathbb{R}^{m \times m}$ ,  $X_2 \in \mathbb{R}^{(n-m) \times m}$  and  $X_3 \in \mathbb{R}^{(n-m) \times (n-m)}$  satisfying the following inequalities:

$$\begin{bmatrix} \text{sym}(ERXL^{-T}) & \text{asym}(ERYL^{-T}) \\ [\alpha - 1] \text{asym}(ERYL^{-T}) & \text{sym}(ERXL^{-T}) \end{bmatrix} \geq 0, \quad (14)$$

$$\text{sym}\{\Theta_\alpha \otimes (A(\alpha_s^{-[\alpha-1]}RXL^{-T} + \alpha_c[\alpha - 1]RYL^{-T}))\} < 0, \quad (15)$$

$$\text{where } X = \begin{bmatrix} \text{sym}(X_1) & 0 \\ X_2 & X_3 \end{bmatrix}, Y = \begin{bmatrix} \text{asym}(X_1) & 0 \\ 0 & 0 \end{bmatrix}.$$

**Proof.** Pre- and postmultiplying (14) by  $\text{diag}(L, L)$  and  $\text{diag}(L^T, L^T)$ , respectively, we have

$$\begin{bmatrix} LERX & LERY \\ [\alpha - 1] LERY & LERX \end{bmatrix} \geq 0, \quad (16)$$

and pre- and postmultiplying (15) by  $\Omega_\alpha \otimes L$  and  $\Omega_\alpha \otimes L^T$ , respectively, we have

$$\text{sym}\{\Theta_\alpha \otimes (LAR(\alpha_s^{-[\alpha-1]}X + \alpha_c[\alpha - 1]Y))\} < 0, \quad (17)$$

where  $\Omega_\alpha = \Omega([\alpha])$ ,  $\Omega(2) = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$  and  $\Omega(1) = 1$ .

Obviously, by Lemmas 3 and 4, when  $0 < \alpha < 1$ , Equations (16) and (17) are equivalent to Equations (7) and (8), respectively, and when  $1 \leq \alpha < 2$ , Equations (16) and (17) are equivalent to Equations (9) and (10), respectively, so Lemmas 3 and 4 are special cases of Theorem 1.  $\square$

**Corollary 1.** System (2) is admissible iff there are  $X_1 \in \mathbb{R}^{m \times m}$ ,  $X_2 \in \mathbb{R}^{(n-m) \times m}$  and  $X_3 \in \mathbb{R}^{(n-m) \times (n-m)}$  satisfying the following inequalities:

$$\begin{bmatrix} \text{sym}(ERXL^{-T}) & \text{asym}(ERXL^{-T}) \\ [\alpha - 1] \text{asym}(ERXL^{-T}) & \text{sym}(ERXL^{-T}) \end{bmatrix} \geq 0, \quad (18)$$

$$\text{sym}\{\Theta_\alpha \otimes (A(\alpha_s^{-[\alpha-1]}R(X + Y)L^{-T} + \alpha_c[\alpha - 1]R(X - Y)L^{-T}))\} < 0, \quad (19)$$

$$\text{where } X = \begin{bmatrix} X_1 & 0 \\ X_2 & X_3 \end{bmatrix}, Y = \begin{bmatrix} X_1^T & 0 \\ X_2 & X_3 \end{bmatrix}.$$

**Proof.** The proof's method is similar to that of Theorem 1, so we omitted it.  $\square$

However, as mentioned in the introduction, the equality constraints in Theorem 1 do not fit; due to the rounding error in the actual calculation, the constraint equation cannot be fully satisfied. Therefore, to improve the accuracy of the calculations, it is better to adopt strict LMI conditions, as shown in Corollary 2.

**Corollary 2.** System (2) is admissible iff there are  $X \in \mathbb{R}^{n \times n}$  and  $Q \in \mathbb{R}^{(n-m) \times n}$  satisfying (4) and

$$\text{sym}\{\Theta_\alpha \otimes (A(X_\alpha E^T + E_0 Q))\} < 0, \quad (20)$$

where  $E_0 \in \mathbb{R}^{n \times (n-m)}$  is an arbitrary column full-rank matrix and satisfies  $EE_0 = 0$ .

**Proof.** (Sufficiency) Suppose that there are two matrices  $X \in \mathbb{R}^{n \times n}$  and  $Q \in \mathbb{R}^{(n-m) \times n}$  that satisfy Equations (4) and (20). Set

$$R\tilde{X}L^{-T} = \text{sym}(X)E^T + (1 - \alpha_c \lfloor \alpha - 1 \rfloor) \alpha_s^{\lfloor \alpha - 1 \rfloor} E_0 Q, R\tilde{Y}L^{-T} = \text{asym}(X)E^T + E_0 Q.$$

It turns out that  $\tilde{X}$  and  $\tilde{Y}$  satisfy Equations (14) and (15). Therefore, from Theorem 1, system (2) is admissible.

(Necessity) Suppose system (2) is admissible. Then, from Lemma 2, there exist two invertible matrices  $L$  and  $R$  that satisfy Equation (6). As system (2) is regular and impulse-free, then  $A_{22}$  is invertible. According to the property of a block matrix, there are two invertible matrices  $L_1$  and  $R_1$ , such that

$$L_1 E R_1 = \begin{bmatrix} I_m & 0 \\ 0 & 0 \end{bmatrix}, L_1 A R_1 = \begin{bmatrix} \bar{A}_{11} & 0 \\ 0 & I_{n-m} \end{bmatrix}.$$

Therefore, system (2) is rewritten as follows

$$\begin{aligned} D^\alpha y_1(t) &= \bar{A}_{11} y_1(t), \\ 0 &= y_2(t), \end{aligned}$$

where  $y_1(t) \in \mathbb{R}^m$ ,  $R_1^{-1} x(t) = [y_1^T(t) \ y_2^T(t)]^T$ . According to Lemma 1, there is a matrix  $\bar{X} \in \mathbb{R}^{m \times m}$  that satisfies (4) and

$$\text{sym}\{\Theta_\alpha \otimes (\bar{A}_{11}(\alpha_s^{-\lfloor \alpha - 1 \rfloor}) \cdot \text{sym}(\bar{X}) + \alpha_c \lfloor \alpha - 1 \rfloor \cdot \text{asym}(\bar{X}))\} < 0.$$

Choose  $E_0$  as

$$E_0 = R_1 \begin{bmatrix} 0 \\ I_{n-m} \end{bmatrix} N,$$

where  $N$  is an arbitrary invertible matrix, and set

$$X = R_1 \begin{bmatrix} \bar{A}_{11} & 0 \\ 0 & I_{n-m} \end{bmatrix} R_1^T, Q = N^{-1} [0 \ -I_{n-m}] L_1^{-T}.$$

Then matrices  $X$  and  $Q$  satisfy Equations (4) and (20).  $\square$

Although Corollary 2 is theoretically a necessary and sufficient condition to judge that system (2) is admissible, unfortunately, Corollary 2 has the disadvantage of dealing with more solved variables, which gives rise to more complex calculations. To overcome this, the following result comes with fewer limitations.

**Theorem 2.** System (2) is admissible iff there are  $X_1 \in \mathbb{R}^{m \times m}$ ,  $X_2 \in \mathbb{R}^{(n-m) \times m}$  and  $X_3 \in \mathbb{R}^{(n-m) \times (n-m)}$  satisfying the following inequalities:

$$\begin{bmatrix} \text{sym}(X_1) & \text{asym}(X_1) \\ \lfloor \alpha - 1 \rfloor \text{asym}(X_1) & \text{sym}(X_1) \end{bmatrix} > 0, \tag{21}$$

$$\text{sym}\{\Theta_\alpha \otimes (L A R (\alpha_s^{-\lfloor \alpha - 1 \rfloor}) X + \alpha_c \lfloor \alpha - 1 \rfloor Y)\} < 0, \tag{22}$$

where

$$X = \begin{bmatrix} \text{sym}(X_1) & 0 \\ X_2 & X_3 \end{bmatrix}, Y = \begin{bmatrix} \text{asym}(X_1) & 0 \\ 0 & 0 \end{bmatrix}, \tag{23}$$

and  $L, R \in \mathbb{R}^{n \times n}$  are given in Lemma 2.

**Proof.** When  $0 < \alpha < 1$ , considering Equations (21) and (22), we easily see that

$$\begin{bmatrix} \text{sym}(X_1) & \text{asym}(X_1) \\ -\text{asym}(X_1) & \text{sym}(X_1) \end{bmatrix} > 0,$$

and

$$\text{sym}\{LAR(\alpha_s X - \alpha_c Y)\} < 0.$$

These two inequalities have the same form as (11) and (12). We easily conclude that Lemma 5 is equivalent to Theorem 2.

When  $1 < \alpha < 2$ , similar to Lemma 5, we easily generalize that system (2) with order  $\alpha$  in (1,2) is admissible iff there exist three matrices  $X_1 \in \mathbb{R}^{m \times m}$ ,  $X_2 \in \mathbb{R}^{(n-m) \times m}$  and  $X_3 \in \mathbb{R}^{(n-m) \times (n-m)}$  such that the following inequalities hold:

$$X_1 > 0, \quad (24)$$

$$\text{sym}\{\Theta \otimes (LARX)\} < 0, \quad (25)$$

where  $X$  is given by Lemma 5.

Equations (21) and (22) are rewritten as follows

$$\begin{bmatrix} X_1 & 0 \\ 0 & X_1 \end{bmatrix} > 0,$$

and

$$\text{sym}\{\Theta \otimes (LARX)\} < 0.$$

From the above two inequalities, it is obvious that the forms of (21) and (22) are the same as those of (24) and (25).

When  $\alpha = 1$ , from Equations (21) and (22), we have

$$\begin{bmatrix} X_1 & 0 \\ 0 & X_1 \end{bmatrix} > 0,$$

and

$$\text{sym}\{LARX\} < 0.$$

Then, it follows that Equations (21) and (22) are equivalent to the Lyapunov stability theorem of singular IOSs.  $\square$

**Remark 1.** The conditions of Corollary 2 and Theorem 2 are strict LMI formulations, which are easier to deal with in the simulation process than those of Theorem 1. More specifically, compared with [29], Theorem 2 does not need to introduce  $E_0$  which satisfies  $EE_0 = 0$  and can avoid the singularity problem caused by variable  $Q$ .

### 3.2. Stabilization of Singular FOS with Order $0 < \alpha < 2$

For the closed-loop system in (27), designing a controller to ensure its admissibility is significant. For further research, we designed the following state feedback controller for system (1):

$$u(t) = Kx(t), K \in \mathbb{R}^{p \times n}, \quad (26)$$

such that the corresponding closed-loop system:

$$ED^\alpha x(t) = (A + BK)x(t). \quad (27)$$

is admissible via the designed controller  $K$ .

Let  $Z = K(X_\alpha E^T + E_0 Q)$ , the following result provides the controller gain for the closed-loop system (27) to be admissible.



**Theorem 3.** System (2) is admissible iff there are  $X \in \mathbb{R}^{n \times n}$ ,  $Q \in \mathbb{R}^{(n-m) \times n}$  and  $Z$  satisfying (4), and

$$\text{sym}\{\Theta_\alpha \otimes (A(X_\alpha E^T + E_0 Q) + BZ)\} < 0, \tag{28}$$

where  $E_0$  is defined in Corollary 2. It can be seen from (28) that  $X_\alpha E^T + E_0 Q$  is nonsingular. The gain  $K$  of the state feedback controller is given by the following formula:

$$K = Z(X_\alpha E^T + E_0 Q)^{-1}. \tag{29}$$

**Example 1.** Consider system (1) with fractional order  $\alpha = \frac{1}{2}$ , and

$$E = \begin{bmatrix} 2 & 3 & 0 \\ 0 & 4 & 0 \\ 0 & 3 & 0 \end{bmatrix}, A = \begin{bmatrix} 1 & 2 & 0 \\ -2 & 1 & 0 \\ 0 & 0 & 3 \end{bmatrix}, B = \begin{bmatrix} 1 \\ 0 \\ 1 \end{bmatrix}.$$

From Definition 1, we easily find that system (1) is not admissible because it does not meet the third property in Definition 1. However, we solve Equations (4) and (28) through Theorem 3, and obtain the following feasible solutions:

$$\begin{aligned} X &= \begin{bmatrix} 23.9331 & 6.4789 & 0 \\ 10.7982 & 15.2945 & 0 \\ 0 & 0 & 23.9331 \end{bmatrix}, \\ Q &= [28.2510 \quad 19.5101 \quad -5.0950], \\ Z &= [-163.9005 \quad -45.1619 \quad -8.6482], \\ K &= [-3.9571 \quad 2.3264 \quad -1.2786]. \end{aligned}$$

**Remark 2.** The method proposed in [30,31] cannot deal with the admissibility problem of a class of singular FOSs when the system matrix  $A$  contains eigenvalues on the positive real part, while the method proposed in this paper does not need to consider the range of eigenvalues of the system matrix  $A$  (as shown in Example 1) and is applicable to a wider range.

When the formulations in Theorem 3 are simulated, the singularity of matrix  $X_\alpha E^T + E_0 Q$  may occur; Theorem 3 cannot be used to judge the admissibility of system (27), so the following theorem is proposed to solve the above problem.

Applying Theorem 2 to the closed-loop linear singular FOS (27), we obtain the following result easily.

**Theorem 4.** System (2) is admissible iff there are  $X_1 \in \mathbb{R}^{m \times m}$ ,  $X_2 \in \mathbb{R}^{(n-m) \times m}$ ,  $X_3 \in \mathbb{R}^{(n-m) \times (n-m)}$  and  $Z$  satisfying (21), and

$$\text{sym}\{\Theta_\alpha \otimes (LAR(\alpha_s^{-[\alpha-1]} X + \alpha_c[\alpha-1]Y) + LBZ)\} < 0, \tag{30}$$

where the meaning of  $L$  and  $R$  is the same as that of Theorem 2. The state feedback controller gain  $K$  is given by

$$K = Z(\alpha_s^{-[\alpha-1]} X + \alpha_c[\alpha-1]Y)^{-1} R^{-1}. \tag{31}$$

### 3.3. Quadratic Admissibility of Uncertain Linear Singular FOS with Order $0 < \alpha < 2$

Consider the norm-bounded uncertain linear singular FOS, which is described as

$$ED^\alpha x(t) = (A + \Delta A)x(t) + (B + \Delta B)u(t), \tag{32}$$

where both  $\Delta A$  and  $\Delta B$  are real matrices with appropriate dimensions to represent the uncertainties of system, and these two matrices are time-independent. According to many existing documents, we reduce these two matrices to the following form

$$[\Delta A \quad \Delta B] = PF(\sigma)[Q_1 \quad Q_2],$$

where  $P, Q_1$  and  $Q_2$  are known real constant matrices.  $\sigma \in \Xi, \Xi$  is a compact set in  $\mathbb{R}$ , and  $F(\sigma)$  is a family of matrices satisfying

$$F^T(\sigma)F(\sigma) \leq I.$$

We set  $A_\Delta = A + \Delta A$  and  $B_\Delta = B + \Delta B$ . System (32) described above is simplified as an unforced uncertain singular FOS, which is written in the following form:

$$ED^\alpha x(t) = A_\Delta x(t). \tag{33}$$

To study the properties of uncertain singular FOSs, we introduce two definitions.

**Definition 2** ([24]). For all allowable time-invariant uncertainty  $\Delta A$ , we say that system (33) is quadratically admissible if there exist  $X, Y \in \mathbb{R}^{n \times n}$  satisfying (14) and

$$\text{sym}\{\Theta_\alpha \otimes (A_\Delta(\alpha_s^{-[\alpha-1]}RXL^{-T} + \alpha_c[\alpha - 1]RYL^{-T}))\} < 0. \tag{34}$$

**Definition 3** ([25]). For all allowable time-invariant uncertainty  $\Delta A$ , we say that system (33) is generalized quadratically stable if there are  $X \in \mathbb{R}^{n \times n}, Q \in \mathbb{R}^{(n-m) \times n}$  satisfying (4) and

$$\text{sym}\{\Theta_\alpha \otimes (A_\Delta(X_\alpha E^T + E_0 Q))\} < 0. \tag{35}$$

Now, we are ready to discuss the necessary and sufficient criteria for the quadratic admissibility and generalized quadratic stability of system (33). According to Theorems 1 and 2, respectively, we immediately get the following Theorems.

**Theorem 5.** System (33) is quadratically admissible iff there exist a positive scalar  $\epsilon$  and three matrices  $X_1, X_2$  and  $X_3$  with appropriate dimensions satisfying (14) and

$$\begin{bmatrix} \Pi_1 & * \\ \Omega_\alpha \otimes (Q_1(\alpha_s^{-[\alpha-1]}RXL^{-T} + \alpha_c[\alpha - 1]RYL^{-T})) & -\epsilon\Omega_\alpha \otimes I_3 \end{bmatrix} < 0, \tag{36}$$

where  $\Pi_1 = 2\text{sym}\{\Theta_\alpha \otimes (A(\alpha_s^{-[\alpha-1]}RXL^{-T} + \alpha_c[\alpha - 1]RYL^{-T}))\} + \epsilon\Omega_\alpha \otimes (PP^T), \Omega_\alpha = \Omega([\alpha]), \Omega(2) = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, \Omega(1) = 1$ .

**Proof.** Replacing  $A$  in Theorem 1 with  $A_\Delta$ , Equation (15) becomes

$$\text{sym}\{\Theta_\alpha \otimes ((A + PF(\sigma)Q_1)(\alpha_s^{-[\alpha-1]}RXL^{-T} + \alpha_c[\alpha - 1]RYL^{-T}))\} < 0.$$

Therefore, it follows that

$$\begin{aligned} &\text{sym}\{\Theta_\alpha \otimes (AR(\alpha_s^{-[\alpha-1]}X + \alpha_c[\alpha - 1]Y)L^{-T})\} + \\ &\text{sym}\{(\Theta_\alpha \otimes P)(\Omega_\alpha \otimes F(\sigma))(\Omega_\alpha \otimes (Q_1R(\alpha_s^{-[\alpha-1]}X + \alpha_c[\alpha - 1]Y)L^{-T}))\} < 0. \end{aligned}$$

According to Fact (A.1) in [9], we see that

$$\begin{aligned} &\Pi_1 + \epsilon^{-1}(\Omega_\alpha \otimes (Q_1R(\alpha_s^{-[\alpha-1]}X + \alpha_c[\alpha - 1]Y)L^{-T}))^T \times \\ &(\Omega_\alpha \otimes Q_1R(\alpha_s^{-[\alpha-1]}X + \alpha_c[\alpha - 1]Y)L^{-T}) < 0. \end{aligned}$$

Applying Schur’s complement, it follows that (36) holds.  $\square$

As for the equality constraint problem discussed above, the data of Theorem 5 may have serious deviations in a simulation, so we give the result with the strict LMI form next.

**Corollary 3.** System (33) is quadratically admissible iff there exist a positive scalar  $\epsilon$  and three matrices  $X_1, X_2$  and  $X_3$  with appropriate dimensions that satisfy (21), (23) and

$$\begin{bmatrix} \Pi_2 & * \\ \Omega_\alpha \otimes (Q_1 R(\alpha_s^{-\lfloor \alpha - 1 \rfloor} X + \alpha_c \lfloor \alpha - 1 \rfloor Y)) & -\epsilon \Omega_\alpha \otimes I_3 \end{bmatrix} < 0, \tag{37}$$

where  $\Pi_2 = 2\text{sym}\{\Theta_\alpha \otimes (LAR(\alpha_s^{-\lfloor \alpha - 1 \rfloor} X + \alpha_c \lfloor \alpha - 1 \rfloor Y))\} + \epsilon \Omega_\alpha \otimes (LPP^T L^T)$ .

Next, according to Definition 3, we easily obtain the following necessary and sufficient condition for the generalized quadratic stability.

**Theorem 6.** System (33) is generalized quadratically stable iff there exist a positive scalar  $\epsilon$  and two matrices  $X$  and  $Q$  with appropriate dimensions that satisfy (4) and

$$\begin{bmatrix} \Pi_3 & * \\ \Omega_\alpha \otimes (Q_1(X_\alpha E^T + E_0 Q)) & -\epsilon \Omega_\alpha \otimes I_3 \end{bmatrix} < 0, \tag{38}$$

where  $\Pi_3 = 2\text{sym}\{\Theta_\alpha \otimes (A(X_\alpha E^T + E_0 Q))\} + \epsilon \Omega_\alpha \otimes (PP^T)$ ,  $E_0$  is the same as in Corollary 2.

Now we give the equivalence relationship between quadratic admissibility and generalized quadratic stability.

**Theorem 7.** These two statements are equivalent:

- (i) System (33) is generalized quadratically stable.
- (ii) System (33) is quadratically admissible.

**Proof.** First, assume that condition (i) is satisfied; we set

$$\begin{aligned} \tilde{X} &= R^{-1}\{\text{sym}(X)E^T + (1 - \alpha_c \lfloor \alpha - 1 \rfloor)\alpha_s^{\lfloor \alpha - 1 \rfloor} E_0 Q\}L^T, \\ \tilde{Y} &= R^{-1}\{\text{asym}(X)E^T + E_0 Q\}L^T. \end{aligned}$$

From (4) and (38) in Theorem 6, it is easy to prove that  $\tilde{X}$  and  $\tilde{Y}$  satisfy (14) and (36), that is, they satisfy Theorem 5, so it means that (ii) is derived from (i).

Now, assume that condition (ii) is satisfied. Thanks to Theorem 5, we find that  $\hat{X}, \hat{Y} \in \mathbb{R}^{n \times n}$  and  $\epsilon > 0$  satisfy (14) and (36). By Lemma 2, there exist two invertible matrices  $L$  and  $R$ , such that the following equation holds.

$$\hat{E} = LER = \begin{bmatrix} I_m & 0 \\ 0 & 0 \end{bmatrix}.$$

Denote

$$\begin{aligned} \hat{X} &= \begin{bmatrix} \hat{X}_1 & \hat{X}_2 \\ \hat{X}_3 & \hat{X}_4 \end{bmatrix}, \\ \hat{Y} &= \begin{bmatrix} \hat{X}_5 & \hat{X}_6 \\ \hat{X}_7 & \hat{X}_8 \end{bmatrix}, \end{aligned}$$

and let

$$\hat{A} = LAR, \hat{P} = LP, \hat{Q}_1 = LQ_1R, \hat{I} = LL^T.$$

Pre- and postmultiplying (14) by  $\text{diag}(L, L)$  and  $\text{diag}(L^T, L^T)$ , respectively, it is easy to get

$$\begin{bmatrix} \hat{E}\hat{X} & \hat{E}\hat{Y} \\ [\alpha - 1]\hat{E}\hat{X} & \hat{E}\hat{X} \end{bmatrix} \geq 0,$$

which shows that

$$\begin{bmatrix} \hat{X}_1 & \hat{X}_5 \\ [\alpha - 1]\hat{X}_5 & \hat{X}_1 \end{bmatrix} > 0.$$

Pre- and postmultiplying (36) by  $\text{diag}(\Omega_\alpha \otimes L, \Omega_\alpha \otimes L)$  and  $\text{diag}(\Omega_\alpha \otimes L^T, \Omega_\alpha \otimes L^T)$ , respectively, we have

$$\begin{bmatrix} \Pi_4 & * \\ \Omega_\alpha \otimes (\hat{Q}_1(\alpha_s^{-[\alpha-1]}\hat{X} + \alpha_c[\alpha - 1]\hat{Y})) & -\epsilon\Omega_\alpha \otimes \hat{I} \end{bmatrix} < 0,$$

where  $\Pi_4 = 2\text{sym}\{\Theta_\alpha \otimes (\hat{A}(\alpha_s^{-[\alpha-1]}\hat{X} + \alpha_c[\alpha - 1]\hat{Y}))\} + \epsilon\Omega_\alpha \otimes (\hat{P}\hat{P}^T)$ . Set

$$\begin{aligned} \hat{E}_0 &= \begin{bmatrix} 0 \\ I_{n-m} \end{bmatrix}, \text{sym}(\Lambda) = \begin{bmatrix} \hat{X}_1 & 0 \\ 0 & I_{n-m} \end{bmatrix}, \text{asym}(\Lambda) = \begin{bmatrix} \hat{X}_5 & 0 \\ 0 & 0 \end{bmatrix}, \\ \hat{Q} &= \begin{bmatrix} \alpha_s^{-[\alpha-1]}\hat{X}_3 + \alpha_c[\alpha - 1]\hat{X}_7 & \alpha_s^{-[\alpha-1]}\hat{X}_4 + \alpha_c[\alpha - 1]\hat{X}_8 \end{bmatrix}. \end{aligned}$$

Therefore, the last inequality becomes

$$\begin{bmatrix} \Pi_5 & * \\ \Omega_\alpha \otimes (\hat{Q}_1((\alpha_s^{-[\alpha-1]} \cdot \text{sym}(\Lambda) + \alpha_c[\alpha - 1] \cdot \text{asym}(\Lambda))\hat{E}^T + \hat{E}_0\hat{Q})) & -\epsilon\Omega_\alpha \otimes \hat{I} \end{bmatrix} < 0,$$

where  $\Pi_5 = 2\text{sym}\{\Theta_\alpha \otimes (\hat{A}((\alpha_s^{-[\alpha-1]} \cdot \text{sym}(\Lambda) + \alpha_c[\alpha - 1] \cdot \text{asym}(\Lambda))\hat{E}^T + \hat{E}_0\hat{Q}))\} + \epsilon\Omega_\alpha \otimes (\hat{P}\hat{P}^T)$ ,  $\Lambda_\alpha = \alpha_s^{-[\alpha-1]}\text{sym}(\Lambda) + \alpha_c[\alpha - 1]\text{asym}(\Lambda)$ .

Let  $E_0 = R\hat{E}_0U$ , and  $U$  is obviously a nonsingular matrix of order  $n - m$ . Denoting

$$\text{sym}(X) = R\text{sym}(\Lambda)R^T, \text{asym}(X) = R\text{asym}(\Lambda)R^T, Q = U^{-1}\hat{Q}L^{-T},$$

and substituting

$$\hat{Q}_1 = LQR, \hat{Q} = UQL^T, \hat{E}_0 = R^{-1}E_0U^{-1}, \hat{P} = LP, \hat{I} = LL^T$$

into the last inequality, gives

$$H \begin{bmatrix} \Pi_3 & * \\ \Omega_\alpha \otimes (Q_1(X_\alpha E^T + E_0Q)) & -\epsilon\Omega_\alpha \otimes I_3 \end{bmatrix} H^T < 0,$$

where  $H = \begin{bmatrix} \Omega_\alpha \otimes L & 0 \\ 0 & \Omega_\alpha \otimes L \end{bmatrix}$  and  $\Pi_3 = 2\text{sym}\{\Theta_\alpha \otimes (A(X_\alpha E^T + E_0Q))\} + \epsilon\Omega_\alpha \otimes (PP^T)$ . Therefore, (4) and (38) hold, so it is proved that (i) is indeed deduced from (ii).  $\square$

When we apply the controller in (26) to system (32), the following closed-loop singular system is easily obtained:

$$ED^\alpha x(t) = (A_\Delta + B_\Delta K)x(t). \tag{39}$$

For uncertain closed-loop singular system (39), let  $F = KR(\alpha_s^{-[\alpha-1]}X + \alpha_c[\alpha - 1]Y)$ , the quadratic admissibility is discussed with the help of Corollary 3.

**Theorem 8.** System (39) is quadratically admissible iff there exist a positive scalar  $\epsilon$  and four matrices  $X_1, X_2, X_3$  and  $F$  with appropriate dimensions that satisfy (21), (23) and

$$\begin{bmatrix} \Pi_6 & * \\ \Omega_\alpha \otimes (Q_1R(\alpha_s^{-[\alpha-1]}X + \alpha_c[\alpha - 1]Y) + Q_2F) & -\epsilon\Omega_\alpha \otimes I_3 \end{bmatrix} < 0, \tag{40}$$

where  $\Pi_6 = 2\text{sym}\{\Theta_\alpha \otimes (LAR(\alpha_s^{-\lfloor \alpha-1 \rfloor} X + \alpha_c \lfloor \alpha-1 \rfloor Y) + LBF)\} + \epsilon \Omega_\alpha \otimes (LPP^T L^T)$ . Then, we design a controller gain  $K$  similar to (31) for system:

$$K = F(\alpha_s^{-\lfloor \alpha-1 \rfloor} X + \alpha_c \lfloor \alpha-1 \rfloor Y)^{-1} R^{-1}. \quad (41)$$

Since the equivalence between quadratic admissibility and generalized quadratic stability has been proved above, letting  $G = K(X_\alpha E^T + E_0 Q)$ , the quadratic admissibility of uncertain closed-loop singular system (39) is obtained directly by using Theorem 6.

**Theorem 9.** System (39) is quadratically admissible iff there exist a positive scalar  $\epsilon$  and two matrices  $X$  and  $G$  with appropriate dimensions that satisfy (4) and

$$\begin{bmatrix} \Pi_7 & * \\ \Omega_\alpha \otimes (Q_1(X_\alpha E^T + E_0 Q) + Q_2 G) & -\epsilon \Omega_\alpha \otimes I_3 \end{bmatrix} < 0, \quad (42)$$

where  $\Pi_7 = 2\text{sym}\{\Theta_\alpha \otimes (A(X_\alpha E^T + E_0 Q) + BG)\} + \epsilon \Omega_\alpha \otimes (PP^T)$ . Then, we design a controller gain  $K$  similar to (29) for the system:

$$K = G(X_\alpha E^T + E_0 Q)^{-1}. \quad (43)$$

#### 4. Numerical Examples

**Example 2.** Consider system (2) with fractional order  $\alpha = \frac{1}{3}, 1$  and  $\frac{4}{3}$ , respectively, and

$$E = \begin{bmatrix} 1 & 2 & 0 \\ 1 & 2 & 0 \\ 0 & 0 & 1 \end{bmatrix}, A = \begin{bmatrix} -2 & 3 & 0 \\ -1 & -2 & 1 \\ 0 & 0 & -1 \end{bmatrix}.$$

By Definition 1, it is easy to verify that when  $\alpha = \frac{1}{3}, 1$  and  $\frac{4}{3}$ , respectively, system (2) is not only regular and impulse-free, but also stable, which shows that system (2) is admissible.

From Theorem 2, we easily use the following commands in MATLAB to find the matrices  $L$  and  $R$ .

```
>> n=3; op=rref([E,eye(n)]); L=op(:,n+1:2*n);
y=op(:,1:n)'; z=rref([y,eye(n)]); R=z(:,n+1:2*n)';
```

After using the above commands, the output results of  $L$  and  $R$  are:

$$L = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & -1 & 0 \end{bmatrix}, R = \begin{bmatrix} 0 & 0 & 1 \\ 0.5 & 0 & -0.5 \\ 0 & 1 & 0 \end{bmatrix}.$$

By substituting these known data into Equations (21) and (22), we find the following feasible solutions:

$$\text{Case } \alpha = \frac{1}{3},$$

$$X = \begin{bmatrix} 0.9620 & 0.0092 & 0 \\ 0.0092 & 0.9151 & 0 \\ 0.6946 & -0.2298 & 0.4962 \end{bmatrix},$$

$$Y = \begin{bmatrix} 0 & -0.0203 & 0 \\ 0.0203 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix};$$

Case  $\alpha = 1$ ,

$$X = \begin{bmatrix} 49.2197 & 6.3283 & 0 \\ 6.3283 & 42.1883 & 0 \\ 33.3489 & -7.5336 & 13.4601 \end{bmatrix},$$

$$Y = 0;$$

Case  $\alpha = \frac{4}{3}$ ,

$$X = \begin{bmatrix} 31.6679 & 4.2297 & 0 \\ 4.2297 & 24.6306 & 0 \\ 21.4115 & -4.0161 & 9.2372 \end{bmatrix},$$

$$Y = 0.$$

**Example 3.** Consider system (1) with fractional order  $\alpha = \frac{1}{2}, 1$  and  $\frac{3}{2}$ , respectively, and

$$E = \begin{bmatrix} 1 & 3 & 7 \\ -1 & 4 & 4 \\ 1 & 10 & 18 \end{bmatrix}, A = \begin{bmatrix} 8 & 9 & 3 \\ 9 & 6 & 5 \\ 2 & 1 & 9 \end{bmatrix}, B = \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}.$$

From Definition 1, we easily find that system (1) is not admissible because it does not meet the third property in Definition 1, i.e., system (1) is not stable. Therefore, we solve Equations (4) and (28) through Theorem 3 (Appendix A), and obtain the following feasible solutions:

Case  $\alpha = \frac{1}{2}$ ,

$$X = \begin{bmatrix} 30.7676 & 3.3166 & -6.2782 \\ 2.0300 & 35.6899 & 4.4758 \\ -8.2999 & 7.4166 & 28.4777 \end{bmatrix},$$

$$Q = [155.8078 \quad 122.1702 \quad 154.7036],$$

$$Z = 10^3 [-2.9445 \quad -1.9258 \quad -3.6030],$$

$$K = [-17.3195 \quad -4.5623 \quad -2.2578];$$

Case  $\alpha = 1$ ,

$$X = \begin{bmatrix} 23.8844 & 2.7622 & -7.5314 \\ 2.7622 & 28.9704 & 6.1439 \\ -7.5314 & 6.1439 & 21.5184 \end{bmatrix},$$

$$Q = [874.8722 \quad 837.5150 \quad 870.8511],$$

$$Z = 10^4 [-1.0277 \quad -0.8163 \quad -0.3391],$$

$$K = [-42.2955 \quad 26.7804 \quad -11.0840];$$

Case  $\alpha = \frac{3}{2}$ ,

$$X = \begin{bmatrix} 17.2252 & 6.3095 & -4.1940 \\ 6.3095 & 16.9514 & 4.2915 \\ -4.1940 & 4.2915 & 20.5553 \end{bmatrix},$$

$$Q = [13.2372 \quad 4.4887 \quad 39.2971],$$

$$Z = 10^3 [-1.4609 \quad -0.9882 \quad -3.9365],$$

$$K = [-4.6030 \quad -3.7138 \quad -6.9714].$$

Using the method of obtaining  $L$  and  $R$  in Example 2, we have

$$L = \begin{bmatrix} 0 & -0.7143 & 0.2857 \\ 0 & 0.0714 & 0.0714 \\ 1 & 0.5 & -0.5 \end{bmatrix}, R = \begin{bmatrix} 0 & 0 & 1 \\ -0.6875 & 1 & 0.6875 \\ 0.4375 & 0 & -0.4375 \end{bmatrix}.$$

Through Theorem 4, we solve Equations (21) and (30) to obtain feasible solutions with fewer solving variables:

$$\text{Case } \alpha = \frac{1}{2},$$

$$X = \begin{bmatrix} 75.3195 & -3.5341 & 0 \\ -3.5341 & 68.8120 & 0 \\ 112.5947 & -3.9036 & -86.8202 \end{bmatrix},$$

$$Y = \begin{bmatrix} 0 & -0.8505 & 0 \\ 0.8505 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix},$$

$$Z = 10^3[-1.0893 \quad -0.6363 \quad 1.0997],$$

$$K = [-12.3951 \quad -13.8790 \quad -9.1984];$$

$$\text{Case } \alpha = 1,$$

$$X = \begin{bmatrix} 167.8076 & -4.7882 & 0 \\ -4.7882 & 158.9910 & 0 \\ 177.4157 & -16.0286 & -24.2666 \end{bmatrix},$$

$$Y = 0,$$

$$Z = 10^3[-2.1074 \quad -1.5873 \quad 0.3052],$$

$$K = [-12.1590 \quad -11.2386 \quad -16.7072];$$

$$\text{Case } \alpha = \frac{3}{2},$$

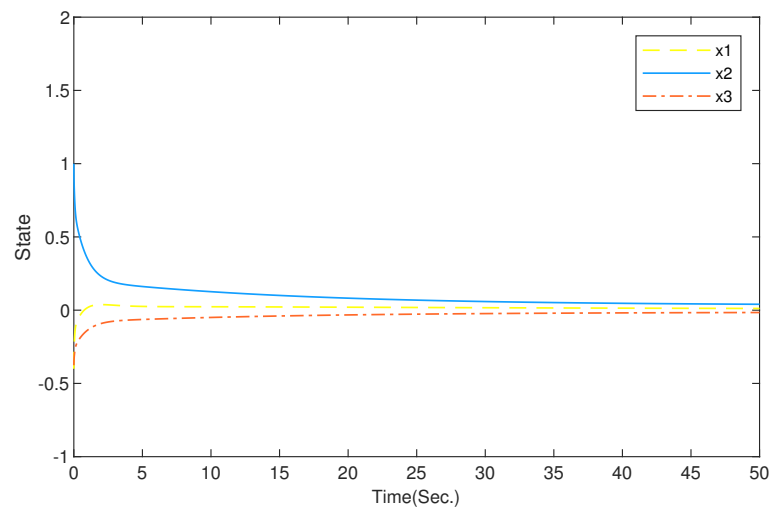
$$X = \begin{bmatrix} 27.5391 & 1.0105 & 0 \\ 1.0105 & 17.7305 & 0 \\ 15.5955 & 7.7775 & -1.8926 \end{bmatrix},$$

$$Y = 0,$$

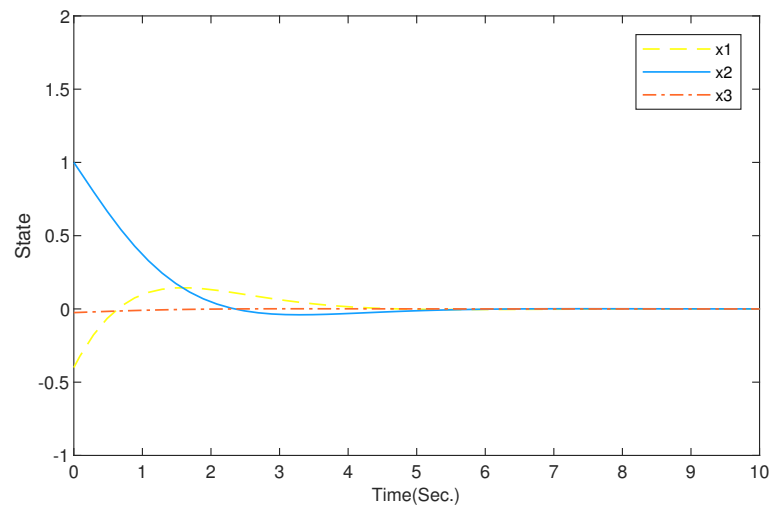
$$Z = [-98.2770 \quad -338.3287 \quad 7.4578],$$

$$K = [-4.6423 \quad -17.3133 \quad -28.8108].$$

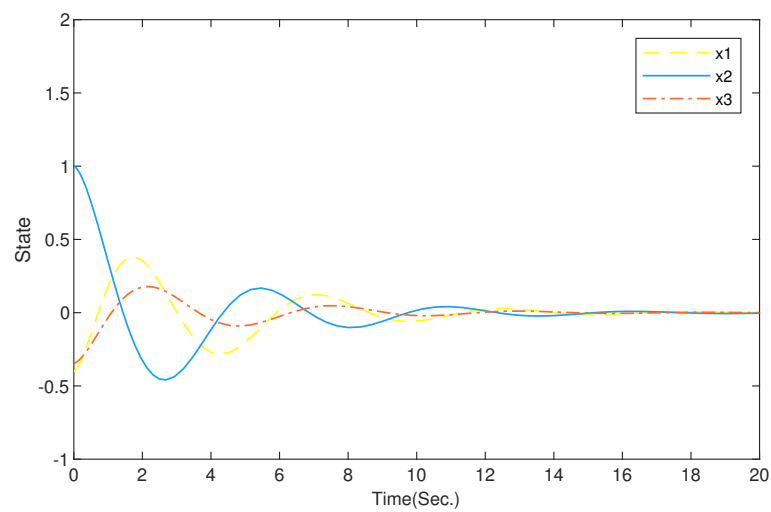
According to the data provided by the above simulation, we describe the state response when  $\alpha$  takes different values through Figures 1–3. Obviously, although the original open-loop systems are not admissible, the corresponding closed-loop systems are admissible under the influence of the control law (26) and reach stability in 50 s, 5 s, and 14 s, respectively.



**Figure 1.** Time response of the closed-loop singular FOS with order  $\alpha = \frac{1}{2}$ .



**Figure 2.** Time response of the closed-loop singular FOS with order  $\alpha = 1$ .



**Figure 3.** Time response of the closed-loop singular FOS with order  $\alpha = \frac{3}{2}$ .



**Example 4.** Consider system (39) with fractional order  $\alpha = \frac{1}{2}, 1$  and  $\frac{7}{6}$ , respectively, and

$$F(\sigma) = \text{diag}(\sin(0.1\text{rand}(1)), e^{-0.5\text{rand}(1)}, \cos(0.5\text{rand}(1)), \sin(0.2\text{rand}(1)) \cos(0.2\text{rand}(1))),$$

$$E = \begin{bmatrix} 2 & 1 & 1 & 1 \\ 2 & 4 & 3 & 5 \\ 0 & -8 & 2 & 3 \\ -2 & -1 & -1 & -1 \end{bmatrix}, A = \begin{bmatrix} 8 & 9 & 6 & 12 \\ -9 & -12 & -5 & -7 \\ 16 & 15 & 3 & 8 \\ -6 & -8 & -5 & -3 \end{bmatrix}, B = \begin{bmatrix} 9 & 6 \\ 7 & -2 \\ 8 & 0 \\ 0 & -1 \end{bmatrix},$$

$$P = \begin{bmatrix} 1 & 1 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 2 \end{bmatrix}, Q_1 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, Q_2 = \begin{bmatrix} 0 & 1 \\ 1 & 0 \\ 0 & -1 \\ 1 & 0 \end{bmatrix}.$$

Using the method of obtaining  $L$  and  $R$  in Example 2, we have

$$L = \begin{bmatrix} 0 & -0.2273 & -0.0227 & -0.7273 \\ 0 & 0.0909 & -0.0909 & 0.0909 \\ 0 & 0.3636 & 0.1364 & 0.3636 \\ 1 & 0 & 0 & 1 \end{bmatrix}, R = \begin{bmatrix} 0 & 0 & 0 & 1 \\ 0.1905 & 1 & 0 & -0.1905 \\ 3.9048 & 0 & 1 & -3.9048 \\ -2.0952 & 0 & 0 & 2.0952 \end{bmatrix}.$$

We easily prove that although system (39) is regular and impulse-free, it is unstable. That is, system (39) is not admissible. Thanks to Theorem 8, we solve Equations (21), (23) and (40), and obtain the following feasible solutions:

Case  $\alpha = \frac{1}{2}$ ,

$$X = \begin{bmatrix} 0.3583 & -0.0676 & -0.1416 & 0 \\ -0.0676 & 0.4546 & -0.1221 & 0 \\ -0.1416 & -0.1221 & 0.5384 & 0 \\ 0.7851 & 0.1576 & 0.0418 & -0.1441 \end{bmatrix},$$

$$Y = \begin{bmatrix} 0 & -0.0295 & 0.0305 & 0 \\ 0.0295 & 0 & 0.0062 & 0 \\ -0.0305 & -0.0062 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix},$$

$$Z = \begin{bmatrix} -0.0482 & -0.0641 & -0.3330 & -0.3320 \\ -0.4203 & -0.4691 & -0.0364 & 0.0256 \end{bmatrix},$$

$$K = \begin{bmatrix} -6.5903 & -3.4565 & -5.1008 & -5.1201 \\ -2.2067 & -1.8261 & -1.1364 & -1.3507 \end{bmatrix},$$

$$\epsilon = 0.8441;$$

Case  $\alpha = 1$ ,

$$X = \begin{bmatrix} 0.3672 & -0.0746 & -0.1970 & 0 \\ -0.0746 & 0.4489 & -0.1387 & 0 \\ -0.1970 & -0.1387 & 0.5868 & 0 \\ 0.7136 & 0.0868 & 0.0091 & -0.1360 \end{bmatrix},$$

$$Y = 0,$$

$$Z = \begin{bmatrix} -0.0415 & -0.0597 & -0.4203 & -0.3937 \\ -0.5122 & -0.5527 & -0.0669 & 0.0723 \end{bmatrix},$$

$$K = \begin{bmatrix} -6.0548 & -3.6073 & -4.6181 & -4.6627 \\ -1.6815 & -1.5876 & -0.8672 & -1.2115 \end{bmatrix},$$

$$\epsilon = 1.0091;$$

$$\text{Case } \alpha = \frac{7}{6},$$

$$X = \begin{bmatrix} 16.2108 & -3.7606 & -14.2136 & 0 \\ -3.7606 & 27.0042 & -12.5891 & 0 \\ -14.2136 & -12.5891 & 43.1088 & 0 \\ 33.1445 & 8.8254 & -6.9612 & -12.5588 \end{bmatrix},$$

$$Y = 0,$$

$$Z = \begin{bmatrix} -3.9891 & -7.8174 & -21.1116 & -15.6831 \\ -19.6255 & -31.9141 & 4.4908 & 8.0433 \end{bmatrix},$$

$$K = \begin{bmatrix} -5.2087 & -3.1530 & -3.3380 & -3.4254 \\ -1.4651 & -1.4050 & -0.6814 & -1.0041 \end{bmatrix},$$

$$\epsilon = 50.3232.$$

It is seen from Figures 4 and 5 that when  $\alpha$  is  $\frac{1}{2}$  and  $\frac{7}{6}$ , respectively, the eigenvalues of the closed-loop systems are in the stability region. That is, although the original open-loop systems are not admissible, their corresponding closed-loop systems are admissible under the influence of the control law (41).

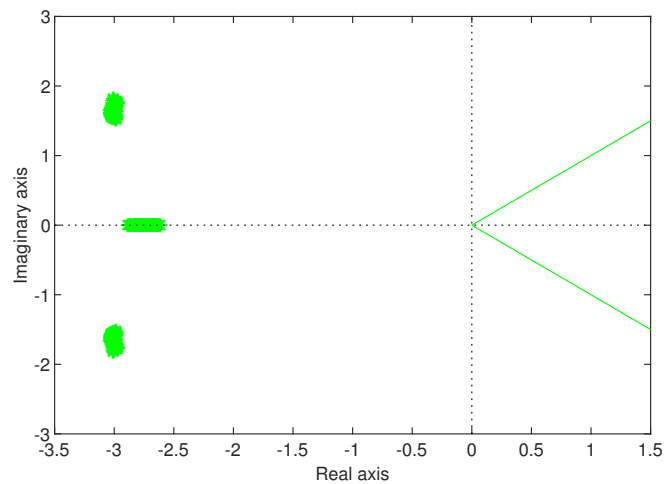


Figure 4. Eigenvalue perturbation region of system with order  $\alpha = \frac{1}{2}$ .

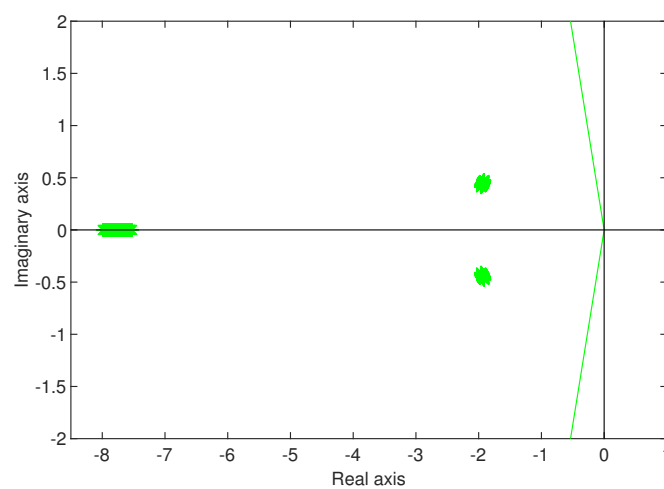


Figure 5. Eigenvalue perturbation region of system with order  $\alpha = \frac{7}{6}$ .

## 5. Conclusions

In this paper, the different necessary and sufficient conditions for the admissibility and quadratic admissibility of a class of singular FOSs with fractional order  $\alpha$  in the interval  $(0, 2)$  were investigated. In order to analyze the admissibility of singular systems, we proposed the methods of LMIs. The state feedback controller was given to solve the problem of quadratic admissibility of norm-bounded uncertain systems with fractional order  $\alpha$  in the range  $0 < \alpha < 2$  without any separation. When  $E = I$  and  $\alpha = 1$ , singular FOSs were simplified into normal FOSs and singular IOSs, respectively. Therefore, these results extended the Lyapunov stability and quadratic admissibility theorem from normal IOSs to singular FOSs with fractional order of  $0 < \alpha < 2$ . In the future, we will further study the  $H_\infty$  control for singular FOSs with order  $0 < \alpha < 2$  and the adaptive-sliding mode fault-tolerant control for interval type-2 fuzzy singular FOSs.

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## Appendix A

The partial LMI algorithm for solving matrices  $X$ ,  $Q$  and  $Z$  with Theorem 3 is given below.

Figure A1 shows a singular FOS model. The module mainly contains the m-function, the fractional-order operator, and the integer-order integrator, the latter two combined into a fractional-order integrator. We adjusted the data in the m-function and integrator according to the simulation needs to get the required relevant data for the singular FOS.

---

### Algorithm A1: The partial LMI algorithm for solving matrices $X$ , $Q$ and $Z$ with Theorem 3

---

```

1 if alpha>0 and alpha<=1 then
2   | theta=1
3 else
4   | theta=(alpha_s - alpha_c; alpha_c - alpha_s)
5 mtheta=size(theta,2);
6 le=eye(mtheta);
7 if mtheta==1 then
8   | [X, sX]=lmivar(2,[n n]);
9   | [Q, sQ]=lmivar(2,[n-m,n]);
10  | [Z, sZ]=lmivar(2,[n-m,n]);
11  | bigX=lmivar(3,[sX]);
12  | bigQ=lmivar(3,[sQ]);
13  | bigZ=lmivar(3,[sZ]);
14 else if mtheta==2 then
15  | [X, sX]=lmivar(2,[n n]);
16  | [Q, sQ]=lmivar(2,[n-m,n]);
17  | [Z, sZ]=lmivar(2,[n-m,n]);
18  | bigX=lmivar(3,[sX zeros(n,n);zeros(n,n) sX]);
19  | bigQ=lmivar(3,[sQ zeros(n-m,n);zeros(n-m,n) sQ]);
20  | bigZ=lmivar(3,[sZ zeros(n-m,n);zeros(n-m,n) sZ]);

```

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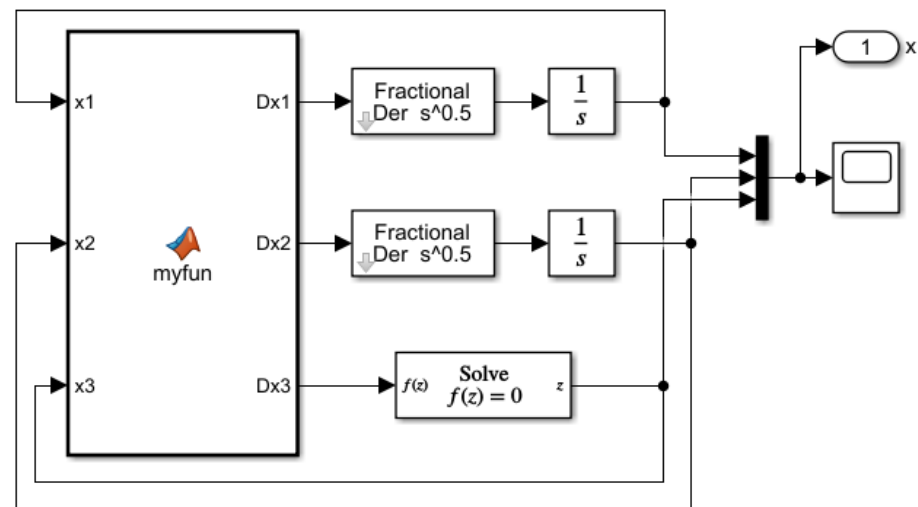


Figure A1. Singular FOS model.

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